## Material and component behavior of light weight steels under complex loadings at high strain rates

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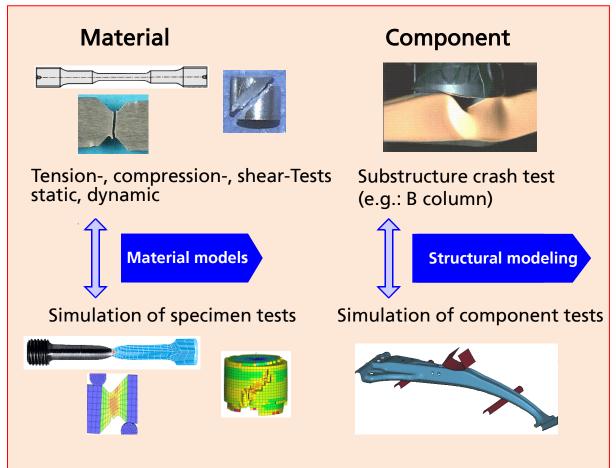


#### **Outline**

- Introduction
- Test equipement for characterization of advanced high strength steel sheets for automotive applications
  - at high strain rates and
  - multiaxial loading conditions
- Experimentally determined material data for simulation
- Modeling
  - Deformation behavior dependent on strain rate
  - Failure behavior dependent on stress state and strain rate
- Model validation with dynamic component tests
- Summary



### Damage concept: multi step evaluation of crashworthiness



#### Vehicle



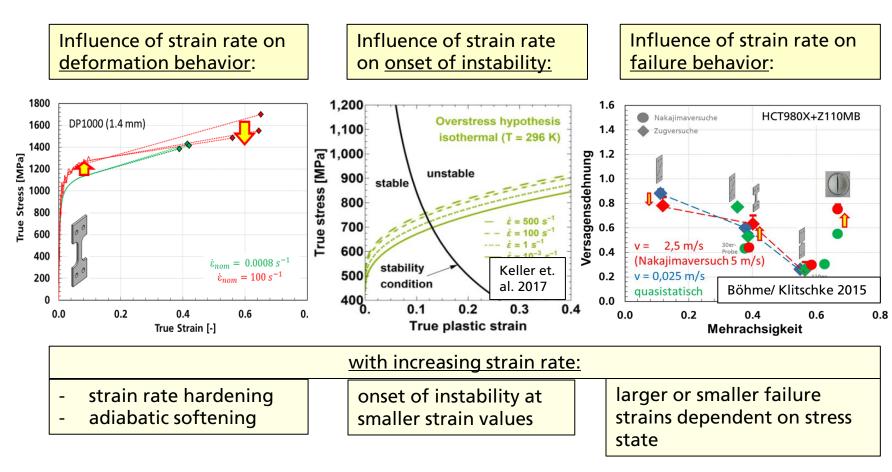
Full scale test



Simulation of Full-Scale Tests



## Influence of strain rate on deformation and failure of advanced high strength steel sheets



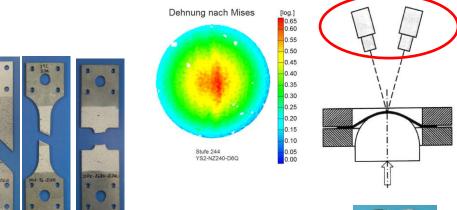


Considering strain rate and stress state in simulation of dynamic loading situations



# Test equipement for specimen tests at high strain rates and multiaxial loading situations

- Servohydraulic high speed testing machine (500 kN / 10 m/s)
- Clamping device for nakajima tests according to DIN EN ISO 12004
- 2 high speed video cameras for 3D-DIC (digital image correlation)



v = 6,25 m/sv = 2,5 m/s  $\dot{\varepsilon} = 250 \text{ s}^{-1}$  $\dot{\varepsilon} = 100 \text{ s}^{-1}$ 

v = 0.025 m/s  $\dot{\epsilon} = 1 \text{ s}^{-1}$ 

v = 0.02 mm/s  $\dot{\epsilon} = 0.0008 \text{ s}^{-1}$ 

v = 0.0015 m/s



v = 5 m/s

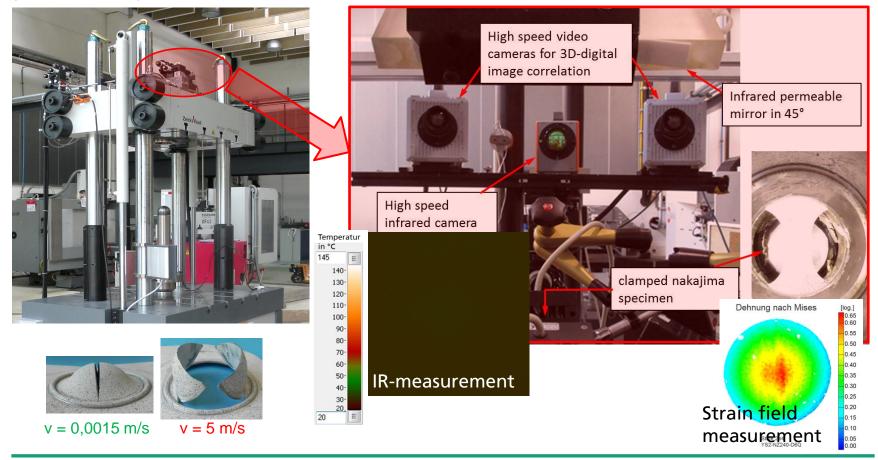




# High speed infrared measurement for nakajima tests on high strength sheet metals at 5 m/s

High speed testing machine (500 kN/10 m/s):

High speed-3D-video recording and infrared measurement with 45° mirror:



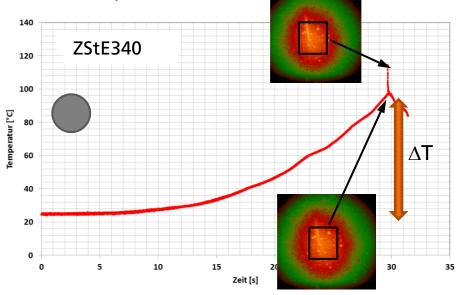
### Adiabatic temperature rise for nakajima tests

### ZStE340, v = 1.5 mm/s und 5 m/s

v = 1.5 mm/s

(Test speed for the determination of forming limits according to DIN EN ISO

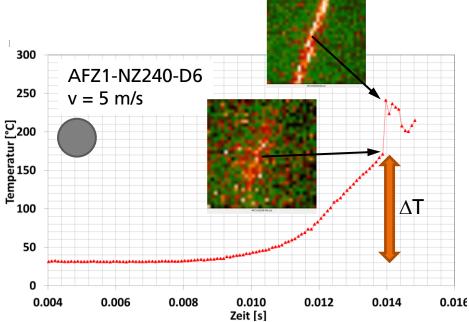
12004-2)



measured <u>maximal</u> temperatur rise in the highly deformed zone immediately before fracture: **70 K**  v = 5 m/s

(local strain rates in the highly deformed

zone ca. 100 s<sup>-1</sup>)

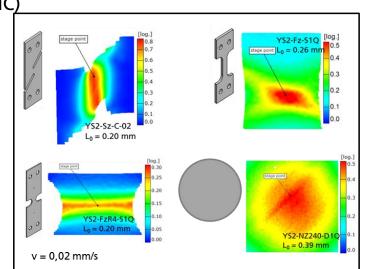


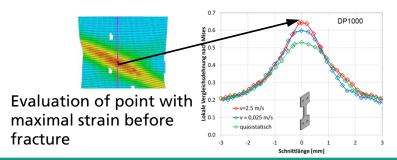
measured <u>maximal</u> temperatur rise in the highly deformed zone immediately before fracture: **140 K** 



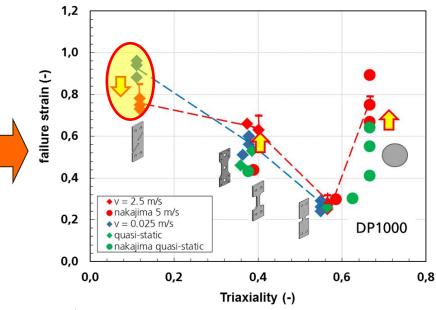
### Failure strains determined by DIC

DP1000: Strain fields immediately before fracture (DIC)





Experimentally determined failure strains:



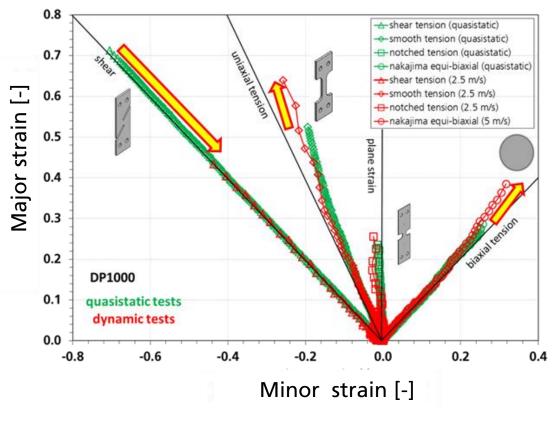
Influence of strain rate on failure strains

Anmerkung: Triaxiality determined by FE-simulation



### Strain paths up to fracture

Evaluation of the time dependent development of major and minor strain up to fracture for a point with maximal strain before fracture:

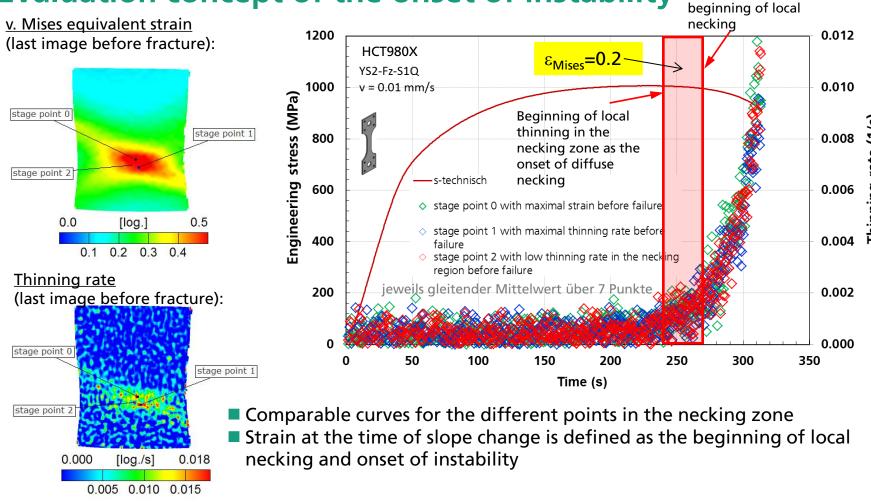




Influence of strain rate on failure strains

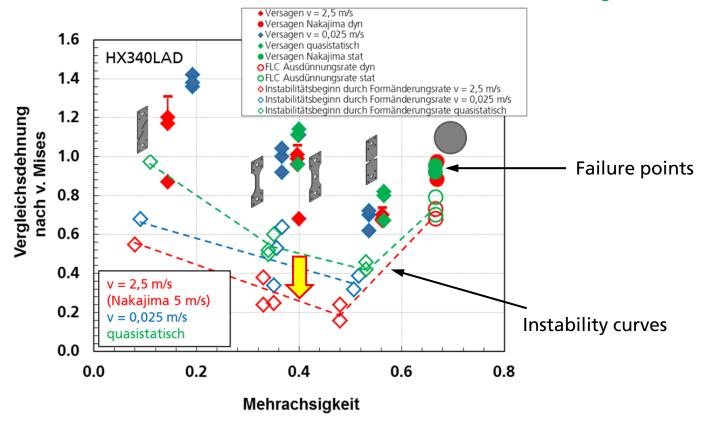


**Evaluation concept of the onset of instability** 



Slope change as the

Influence of strain rate on the onset of instability



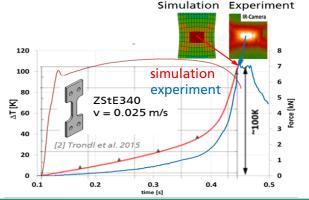
Under dynamic loading tendency of smaller values for strains at the onset of instability compared with quasistatic loading

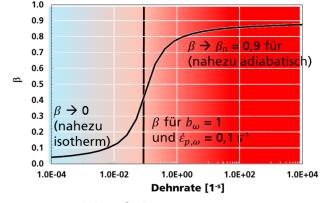


### FE-Simulation: Considering influence of strain rate and stress state on material behavior

### Adiabatic softening (MAT\_TABULATED\_JOHNSON\_COOK)

- Avoiding thermomechanical coupling in simulation with <u>pseudothermomechanical material model</u>
- isotropic thermo-viscoplastic material model with adiabatic softening dependent on strain rate (LS-Dyna, MAT\_224)
- Johnson-Cook-approach:  $\sigma = s(\varepsilon_p, \dot{\varepsilon}_p) \cdot g(T)$ with  $s(\varepsilon_p, \dot{\varepsilon}_p)$ : isothermal flow curves g(T): softening function
- Temperature calculation:  $\dot{T} = \frac{\partial T}{\partial t} = \beta(\dot{\epsilon}_{pl}) \frac{\sigma \dot{\epsilon}}{\rho c_p}$





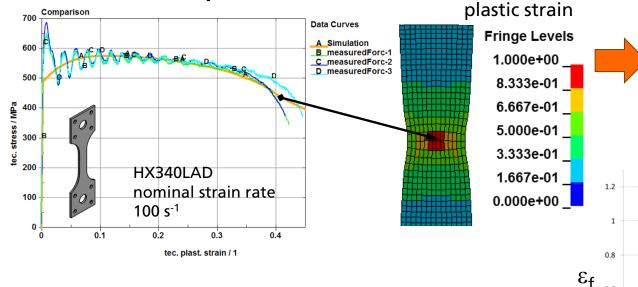
 $b_{\omega}$  - width of the transition region  $\dot{arepsilon}_{p,\omega}$  - "transition strain rate"

- non-isothermal strain rate range: good prediction of material behavior for uniaxial tension
- Influence on stress state on adiabatic softening will be considered in the future

### FE-Simulation: Considering influence of strain rate and stress state on material behavior

Failure, damage (MAT\_ADD\_EROSION, GISSMO)

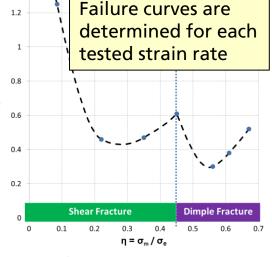
#### 1. Simulation of specimen tests



#### 2. Failure curves

two spline-interpolations for two damage areas of the failure curves (shear failure and dimple fracture)

Comment: Gissmo = Generalized Incremental Stress State dependent damage model (Haufe et. al. 2011)



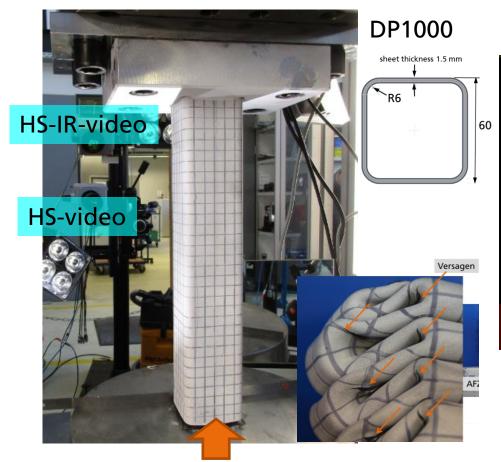
Failure strains

determined by

simulation

#### **Modelvalidation**

### Dynamic component tests (v = 5 m/s)



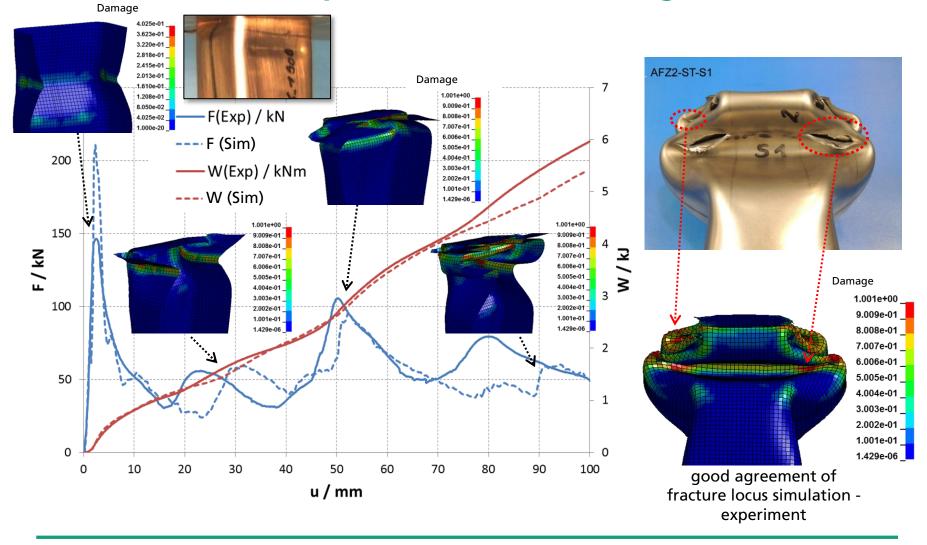
High speed infrared temperatur measurement in °C 220 200 180-160-140-120-100-80-60-40-

Measurement of temperature development

Measurement of force deformation behavior

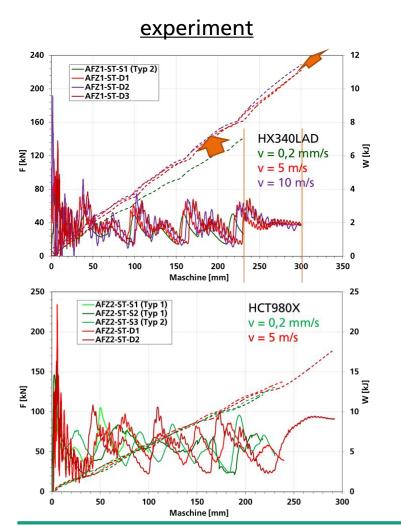
#### **Component tests and simulation**

### HCT980X, Force-displacement, local damage, static

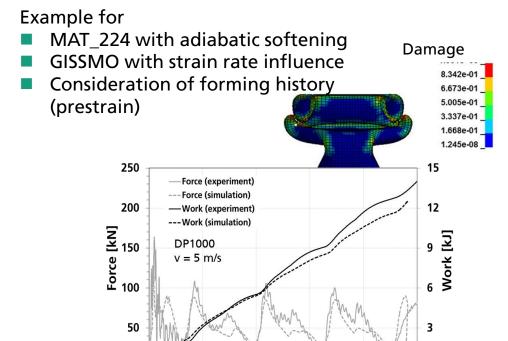


#### **Modelvalidation**

### Energy absorption of dynamically tested component



#### <u>simulation</u>



Under dynamic loading material dependent higher energy absorption compared to quasistatic loading!

100

150

Displacement [mm]

200

50

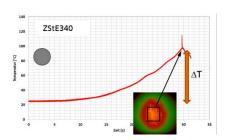
0

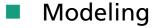


250

#### **Summary**

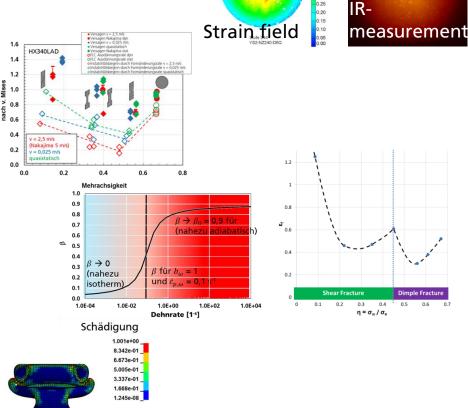
- Specimen tests at high strain rates and different loading situations
  - Strain and temperature field measurement
- Material data for simulation





- Johnson-Cook-model
- Gissmo-failure model
- Modelvalidation





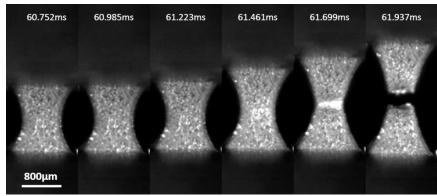


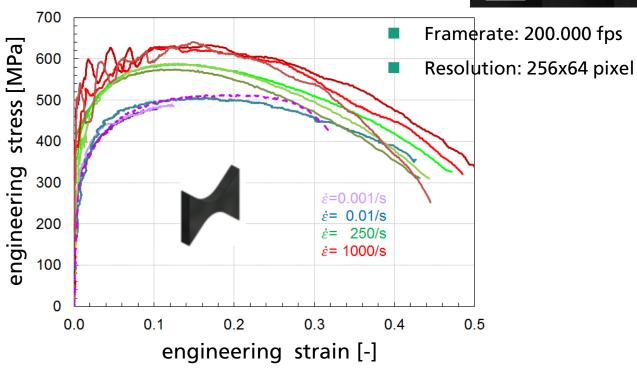
### Perspective: Micro Testing over 5 Strain Rate Decades

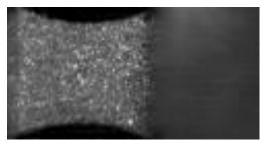
Velocity of testing: 1 m/s

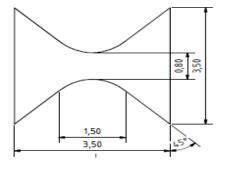
Acceleration: 50 m/s<sup>2</sup>

Framerate: 300.000 fps









Geometry of tested specimen

### **Acknowledgements**

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